

# PERFORMANCE OF THE JOUYBAN-ACREE MODEL FOR CORRELATING THE SOLUBILITY OF INDOMETHACIN AND ETHYLHEXYL TRIAZONE IN ETHYL ACETATE + ETHANOL MIXTURES

DESEMPEÑO DEL MODELO DE JOUYBAN-ACREE EN LA CORRELACIÓN DE LA SOLUBILIDAD DE INDOMETACINA Y ETILHEXIL TRIAZINA EN MEZCLAS ACETATO DE ETILO + ETANOL

Miller A. RUIDIAZ M.<sup>1</sup>, Sylvia J. RODRÍGUEZ D.<sup>1</sup>, Paula C. NEITA R.<sup>1</sup>, Diana M. CRISTANCHO B.<sup>1</sup>, Fleming MARTÍNEZ R.<sup>1\*</sup>

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## ABSTRACT

This work reports the experimental volumetric properties and also the saturated solubility of indomethacin and ethylhexyl triazine in ethyl acetate + ethanol mixtures at 293.15 to 313.15 K and evaluates the validity of the Jouyban-Acree (J & A) model to correlate the solubility of these compounds in ethyl acetate + ethanol solvent mixtures. The solubility correlation is studied as a function of temperature and cosolvent composition. The J & A model requires only the experimental solubility values in the pure solvents at all the temperatures under study. The calculated values by using both compounds deviate as mean in 30% from experimental solubility values.

**Keywords:** Indomethacin, ethylhexyl triazone, solubility, ethanol, ethyl acetate, solvent mixtures, Jouyban-Acree equation.

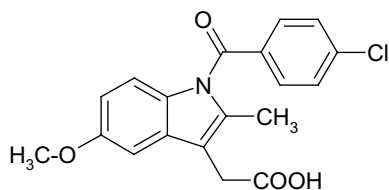
## RESUMEN

En este trabajo se evalúa la validez del modelo de Jouyban-Acree (J – A) para la correlación de la solubilidad de estos dos agentes de uso farmacéutico en mezclas acetato de etilo + etanol, en función de la composición solvente y de la temperatura, en el intervalo entre 293,15 y 313,15 K. El modelo J – A requiere únicamente de los valores experimentales de solubilidad de los fármacos en los solventes puros en función de la temperatura. Se encuentra que los valores obtenidos con los dos compuestos presentan desviaciones cercanas al 30% respecto a los valores experimentales de solubilidad.

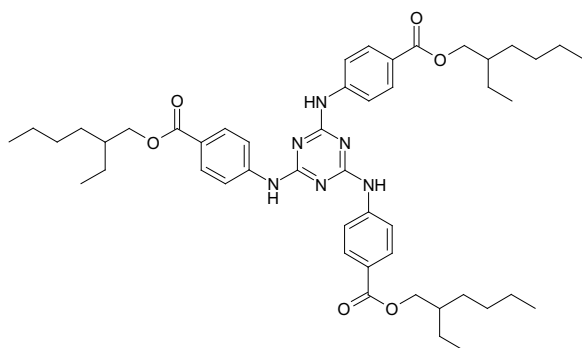
**Palabras clave:** Indometacina, Etilhexil triazina, solubilidad, etanol, acetato de etilo, mezclas de solventes, ecuación de Jouyban-Acree.

## INTRODUCTION

Indomethacin (IMC, molecular structure showed in figure 1) is an anti-inflammatory drug sometimes used in actual therapeutics (1), while ethylhexyl triazone (EHT, molecular structure showed in figure 2) is a sunscreen agent widely used in the formulation of skin care products (2, 3). Physicochemical properties of IMC and EHT have not been thoroughly studied. In this context, it is well known that several physicochemical properties such as, the solubility and occupied volumes by active ingredients and excipients in adequate solutions, are very important for pharmaceutical scientists, because they facilitate the processes associated to design and development of new products in the pharmaceutical and cosmetic industries (4).



**Figure 1.** Molecular structure of indomethacin.



**Figure 2.** Molecular structure of ethylhexyl triazone.

On the other hand, ethyl acetate and ethanol have been widely used in drug microencapsulation processes (5). Moreover, ethyl acetate + ethanol binary system has been widely used as model mixed solvent for solubility studies of several drugs developed by Bustamante *et al* (6-13). Recently, Jouyban and Acree, 2007 (14) have developed a semi-empirical method intended to estimate drugs solubilities in this binary solvent system, whereas Ruidiaz and Martinez, 2009 (15) and Rodríguez *et al.*, 2010 (16) have evaluated the usefulness of the Extended Hildebrand Solubility Approach

to estimate the solubility of indomethacin and ethylhexyl triazone at 298.15 K in the same solvent system, respectively. Ultimately, Ruidiaz *et al.*, 2010 have evaluated the volumetric behavior of this pharmaceutical model solvent system (17). For these reasons, the main objective of this study was to evaluate the usefulness of Jouyban-Acree model (14) to correlate the equilibrium solubility of two pharmaceutical compounds with great difference in molar mass and volume, namely, IMC and EHT, in binary mixtures conformed by ethyl acetate and ethanol as a function of the solvent composition and temperature.

## THEORETICAL ASPECTS

Several methods to estimate the solubility in solvent mixtures have been reported in the pharmaceutical and chemical literature. Some of them have been challenged recently in the correlation of the equilibrium solubility of several drugs (18, 19).

As was already exposed (20), the simplest model to predict drug solubility in mixtures is the one based on the algebraic rule of mixing, which for semipolar compounds in binary mixtures takes the following form:

$$\log X_{3\text{-mix}} = f_1 \log X_{3\text{-solv.1}} + f_2 \log X_{3\text{-solv.2}}$$

### Equation 1.

where  $X_{3\text{-mix}}$  is the calculated solubility of solute in the mixture considered,  $X_{3\text{-solv.1}}$  is the solute solubility in the neat solvent 1,  $X_{3\text{-solv.2}}$  is the solute solubility in the neat solvent 2, and  $f_1$  and  $f_2$  are the volume fractions of both solvents in the mixture free of solute. The first one is calculated, by assuming volumes additivity as follows:

$$f_1 = \frac{V_1}{V_1 + V_2} \quad \text{Equation 2.}$$

where,  $V_1$  and  $V_2$  are the volumes of solvents 1 and 2, respectively (21). It is clear that  $f_2$  is equal to  $1 - f_1$ .

Nevertheless, it was found experimentally that the behavior of several lipophilic solutes deviate notoriously of this simple additive rule of solubility, in particular when the solvents used are amphiprotic. As good attempt to consider the deviations non taken into account by equation 1 Jouyban and Acree proposed the equation 3,

where  $T$  is the absolute temperature and  $J_i$  are the respective polynomial coefficients.  $J_i$  coefficients present theoretical meaning because each one of them is a function of the interaction energies among two and three bodies, which in turn describe the attractions among the different molecules present in solution. Equation 3 is derived from the equation originally proposed by Redlich and Kister, 1948 (22), and its development as well as its meaning has been described previously in the literature (23, 24).

$$\log X_{3\text{-mix}} = f_1 \log X_{3\text{-solv.1}} + f_2 \log X_{3\text{-solv.2}} + \frac{f_1 f_2}{T} \sum_{i=0}^n J (f_1 - f_2)^i \quad \text{Equation 3.}$$

Recently, Jouyban and Acree, 2007 (14) processed by regression analysis the solubility values (as mole fraction) of several drugs in AcOEt + EtOH mixtures reported in the literature (6-13), in front to equation 3, obtaining the equations 4 and 5,

$$\log X_{3\text{-mix}} = f_1 \log X_{3\text{-solv.1}} + f_2 \log X_{3\text{-solv.2}} + J - \text{A Factor} \quad \text{Equation 4.}$$

where the J - A Factor is defined according to the following expression:

$$\text{J - A Factor} = \left( \frac{f_1 f_2}{T} \right) (382.987 + 125.663\{f_1 - f_2\} + 214.579\{f_1 - f_2\}^2) \quad \text{Equation 5.}$$

In equations 4 and 5 the solvent 1 is the one where the solubility is greatest between both neat solvents considered. As examples, for the solubility of caffeine in AcOEt + EtOH mixtures, AcOEt is the solvent 1 and EtOH is the solvent 2, whereas for the solubility of acetaminophen in the same solvent system, EtOH is the solvent 1 and AcOEt is the solvent 2 (14).

## MATERIALS AND METHODS

### Materials

In this investigation the following reagents and materials were used, indomethacin BP (25), ethylhexyl triazone obtained from BASF, ethyl

acetate A.R. Merck (AcOEt), absolute ethanol A.R. Merck (EtOH), molecular sieve Merck (numbers 3 and 4, pore size 0.3 and 0.4 nm, respectively), and Durapore® 0.45  $\mu\text{m}$  filters from Millipore Corp.

### Solvent mixtures preparation

The dehydrated ethanol employed was maintained over molecular sieve (Merck Number 3, 0.3 nm in pore diameter) to obtain a dry solvent previously to prepare the solvent mixtures. The ethanol dryness was demonstrated by the respective density value obtained ( $0.7854 \text{ g cm}^{-3}$  at 298.15 K), which was thus coincident with those reported in the literature (26, 27). All AcOEt + EtOH solvent mixtures were prepared in quantities of 10.00 g by mass using an Ohaus Pioneer TM PA214 analytical balance with sensitivity  $\pm 0.1 \text{ mg}$ , in mass fractions from 0.10 to 0.90 varying by 0.10, in order to study nine mixtures and both pure solvents.

### Solubility determination

An excess of IMC or EHT was added to each organic solvent evaluated in stoppered dark glass flasks. Solid-liquid mixtures were placed on thermostatic baths (Neslab RTE 10 Digital One Thermo Electron Company) kept at temperatures from  $293.15 \pm 0.05 \text{ K}$  to  $313.15 \pm 0.05 \text{ K}$  with sporadic stirring for at least three days to reach the solution equilibrium (this equilibrium time was established by quantifying the IMC or EHT concentration up to obtain constant values). Once at equilibrium, supernatant solutions were filtered (at isothermal conditions) to remove insoluble particles before the respective composition analyses. IMC or EHT concentrations were determined by mass balance by weighing a specified quantity of the respective saturated solution and allowing the solvent evaporation up to constant mass. All the solubility experiments were run at least in triplicate. In order to make the equivalence between volumetric and gravimetric concentration scales, the density of the saturated solutions was determined with a digital density meter (DMA 45 Anton Paar) connected to the same recirculating thermostatic baths.

### Deviations calculation

As a deviation criterion between single experimental and calculated values by equations 1 and 5, the percentage deviations (%D) were calculated considering the unmodified solubility values according to following equation:

$$\%D = 100 \cdot \frac{|X_{3\text{-mix}}^{\text{calc}} - X_{3\text{-mix}}^{\text{expt}}|}{X_{3\text{-mix}}^{\text{expt}}} \quad \text{Equation 6.}$$

On similar way, as a general criterion of the usefulness of both equations the mean percentage deviations ( $M\%D$ ) were calculated by means of the equation 7, where  $n$  is the number of mixtures compositions considered.

$$M\%D = \frac{100}{n} \sum_{i=1}^n \left( \frac{|X_{3\text{-mix}}^{\text{calc}} - X_{3\text{-mix}}^{\text{expt}}|}{X_{3\text{-mix}}^{\text{expt}}} \right) \quad \text{Equation 7.}$$

## RESULTS AND DISCUSSION

It is well known that the volumetric concentration scales depend on temperature varying according to their respective thermal-volume expansion coefficients ( $\alpha$ ). For this reason, table 1 shows the temperature dependence of volume fraction

in AcOEt + EtOH mixtures with the mass composition varying in 0.10 in mass fraction ( $\mu_{\text{AcOEt}}$ ). The respective statistical description is also showed.

Although the  $\alpha$  values for AcOEt and EtOH are slightly different,  $1.397 \times 10^{-3} \text{ K}^{-1}$  and  $1.123 \times 10^{-3} \text{ K}^{-1}$ , respectively (17), the temperature dependence of  $f$  with temperature is relatively low, being in the nine cases lower than 0.19%, which for practical purposes is considered insignificant. Moreover, the mean values obtained are similar to those obtained at 303.15 K. For this reason, in challenging equations 1 to 5 the values obtained at this temperature were used on the same way as it was done in other similar investigations (28-30).

Table 2 shows the experimental values of equilibrium solubility for both pharmaceutical compounds expressed as decimal logarithms of mole fraction. The values used as input in equations 1 to 5 were those obtained in neat solvents at all temperatures.

**Table 1.** Volume fraction of AcOEt in AcOEt + EtOH mixtures as a function of mixtures composition and temperature

$\mu_{\text{AcOEt}}$	$f_{\text{AcOEt}}$						%VC <sup>(b)</sup>
	293.15 K	298.15 K	303.15 K	308.15 K	313.15 K	Mean (SD) <sup>(a)</sup>	
0.1000	0.1125	0.1123	0.1122	0.1120	0.1120	0.1122 (0.0002)	0.19
0.2000	0.2219	0.2216	0.2214	0.2211	0.2210	0.2214 (0.0004)	0.17
0.3000	0.3283	0.3280	0.3277	0.3274	0.3272	0.3277 (0.0005)	0.14
0.4000	0.4319	0.4316	0.4312	0.4309	0.4307	0.4313 (0.0005)	0.12
0.5000	0.5328	0.5325	0.5321	0.5317	0.5315	0.5321 (0.0005)	0.10
0.6000	0.6311	0.6308	0.6304	0.6301	0.6299	0.6305 (0.0005)	0.08
0.7000	0.7269	0.7266	0.7263	0.7260	0.7258	0.7263 (0.0004)	0.06
0.8000	0.8202	0.8200	0.8198	0.8196	0.8194	0.8198 (0.0003)	0.04
0.9000	0.9112	0.9111	0.9110	0.9109	0.9108	0.9110 (0.0002)	0.02

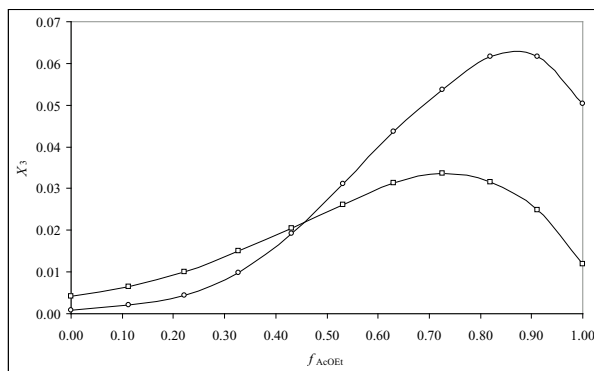
(a) SD is standard deviation. (b) %VC is percentage variation coefficient.

**Table 2.** Experimental solubility of IMC and EHT expressed as decimal logarithm as a function of mixtures composition and temperature. Values in parentheses are percentage variation coefficients on equilibrium solubility.

$\mu_{\text{AcOEt}}$	$f_{\text{AcOEt}}$	293.15 K	298.15 K	303.15 K	308.15 K	313.15 K
IMC						
0.0000	0.0000	-2.479 (1.5)	-2.380 (1.1)	-2.309 (0.4)	-2.208 (0.2)	-2.131 (0.3)
0.1000	0.1122	-2.254 (1.9)	-2.182 (1.1)	-2.106 (0.2)	-2.015 (1.3)	-1.948 (0.2)
0.2000	0.2214	-2.054 (0.8)	-1.998 (2.6)	-1.927 (1.2)	-1.844 (0.6)	-1.785 (0.1)
0.3000	0.3277	-1.884 (0.5)	-1.822 (0.4)	-1.772 (0.4)	-1.703 (0.5)	-1.653 (0.6)
0.4000	0.4312	-1.735 (2.5)	-1.688 (1.8)	-1.639 (1.3)	-1.585 (0.7)	-1.544 (0.7)
0.5000	0.5321	-1.622 (1.8)	-1.581 (1.9)	-1.545 (0.5)	-1.496 (0.1)	-1.463 (0.2)
0.6000	0.6304	-1.542 (2.0)	-1.503 (1.6)	-1.469 (2.6)	-1.432 (0.4)	-1.408 (0.2)
0.7000	0.7263	-1.510 (0.4)	-1.473 (0.6)	-1.442 (0.4)	-1.408 (0.4)	-1.385 (0.3)
0.8000	0.8198	-1.531 (0.1)	-1.502 (0.1)	-1.462 (0.4)	-1.427 (1.1)	-1.399 (0.3)

$\mu_{\text{AcOEt}}$	$f_{\text{AcOEt}}$	293.15 K	298.15 K	303.15 K	308.15 K	313.15 K
IMC						
0.9000	0.9110	-1.646 (0.4)	-1.605 (1.6)	-1.565 (0.6)	-1.527 (0.6)	-1.488 (0.3)
1.0000	1.0000	-1.980 (1.6)	-1.922 (0.2)	-1.862 (2.9)	-1.804 (1.7)	-1.745 (0.6)
EHT						
0.0000	0.0000	-3.153 (1.3)	-3.039 (0.6)	-2.913 (1.3)	-2.731 (1.8)	-2.561 (1.7)
0.1000	0.1122	-2.791 (1.1)	-2.691 (0.3)	-2.562 (0.8)	-2.374 (0.1)	-2.142 (0.8)
0.2000	0.2214	-2.463 (0.8)	-2.348 (0.6)	-2.186 (0.4)	-1.953 (0.8)	-1.716 (0.3)
0.3000	0.3277	-2.122 (0.9)	-2.010 (1.1)	-1.834 (0.3)	-1.612 (1.2)	-1.416 (1.2)
0.4000	0.4312	-1.767 (1.7)	-1.716 (0.6)	-1.553 (1.7)	-1.377 (3.1)	-1.243 (0.3)
0.5000	0.5321	-1.531 (2.1)	-1.506 (0.3)	-1.371 (0.7)	-1.240 (1.2)	-1.138 (0.6)
0.6000	0.6304	-1.364 (1.3)	-1.359 (0.8)	-1.253 (0.4)	-1.142 (2.2)	-1.065 (0.8)
0.7000	0.7263	-1.273 (1.1)	-1.270 (1.3)	-1.179 (0.4)	-1.079 (1.8)	-1.022 (0.1)
0.8000	0.8198	-1.216 (0.5)	-1.211 (0.3)	-1.136 (0.2)	-1.061 (0.2)	-1.001 (0.4)
0.9000	0.9110	-1.221 (1.8)	-1.210 (0.5)	-1.141 (0.8)	-1.061 (1.1)	-0.995 (2.6)
1.0000	1.0000	-1.326 (2.0)	-1.299 (0.6)	-1.214 (0.5)	-1.132 (1.2)	-1.056 (0.1)

On the other hand, figure 3 shows the experimental solubility of both drugs at 298.15 K expressed as mole fraction. It is clear that maximum solubility is obtained in solvent mixtures instead of neat solvents, although the greatest solubility in neat solvents is obtained in AcOEt for both drugs. In this way, for these compounds the solvent 1 is AcOEt and the solvent 2 is EtOH.



**Figure 3.** Experimental solubility expressed as mole fraction of IMC (o) and EHT ( $\square$ ) as a function of AcOEt volume fraction in AcOEt + EtOH mixtures at 298.15 K.

Tables 3 and 4 show the values of logarithmic solubility calculated by means of equations 1 and 4 as a function of mixtures composition and temperature for both drugs, respectively. Individual and group percentage deviations with respect to equilibrium solubilities are also showed in tables 3 and 4. It is important to note that these methods were selected for this study because they are the most simple among those described in the literature (18).

By comparing the predictive results obtained for both drugs it is clear that Jouban-Acree model (equations 4 and 5) is better than additive behavior (equation 1), because of their M%D values, namely,  $29 \pm 13\%$  for IMC and  $33 \pm 17\%$  for EHT in the first case, in front to  $60 \pm 14\%$  for IMC and  $62 \pm 15\%$  for EHT in the case of equation 1. Thus, J – A model would be useful if equilibrium solubility estimations within 30% in uncertainty are allowed.

To see more clearly these effects, figure 4 shows the differences obtained between experimental solubilities for both drugs at 298.15 K in front to those calculated by means of equation 1. figure 4 also shows the differences obtained between equations 1 and 4 (and 5), respectively.

**Table 3.** Solubility of IMC and EHT calculated by means of additive-logarithmic model (equation 1) expressed as decimal logarithm as a function of mixtures composition and temperature. Values in parentheses are percentage deviations calculated according to equation 6.

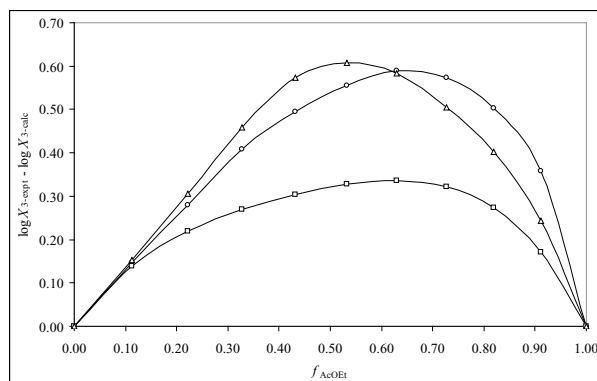
$f_{AcOEt}$	293.15 K	298.15 K	303.15 K	308.15 K	313.15 K	M%D <sup>(a)</sup>
IMC						
0.1122	-2.423 (32.2)	-2.328 (28.7)	-2.259 (29.6)	-2.163 (28.8)	-2.087 (27.5)	29.4 ± 1.7
0.2214	-2.369 (51.5)	-2.278 (47.6)	-2.210 (47.9)	-2.119 (46.9)	-2.045 (45.1)	47.8 ± 2.3
0.3277	-2.316 (63.0)	-2.230 (60.9)	-2.163 (59.3)	-2.076 (57.7)	-2.004 (55.5)	59.3 ± 2.9
0.4312	-2.264 (70.4)	-2.182 (67.9)	-2.116 (66.7)	-2.034 (64.5)	-1.964 (62.0)	66.3 ± 3.2
0.5321	-2.214 (74.4)	-2.136 (72.1)	-2.071 (70.2)	-1.993 (68.2)	-1.926 (65.5)	70.1 ± 3.4
0.6304	-2.165 (76.2)	-2.091 (74.2)	-2.027 (72.4)	-1.954 (69.9)	-1.888 (66.9)	71.9 ± 3.6
0.7263	-2.117 (75.3)	-2.047 (73.3)	-1.984 (71.3)	-1.915 (68.9)	-1.851 (65.8)	70.9 ± 3.7
0.8198	-2.070 (71.1)	-2.004 (68.6)	-1.942 (66.9)	-1.877 (64.5)	-1.815 (61.6)	66.5 ± 3.7
0.9110	-2.025 (58.2)	-1.963 (56.1)	-1.902 (54.0)	-1.840 (51.4)	-1.779 (48.9)	53.7 ± 3.7
						60 ± 14
EHT						
0.1122	-2.948 (30.3)	-2.843 (29.5)	-2.722 (30.8)	-2.552 (33.6)	-2.392 (43.7)	33.6 ± 5.9
0.2214	-2.749 (48.2)	-2.653 (50.5)	-2.537 (55.4)	-2.377 (62.4)	-2.228 (69.2)	57.1 ± 8.7
0.3277	-2.554 (63.1)	-2.468 (65.2)	-2.356 (70.0)	-2.207 (74.6)	-2.068 (77.7)	70.1 ± 6.2
0.4312	-2.365 (74.8)	-2.288 (73.2)	-2.180 (76.4)	-2.042 (78.4)	-1.912 (78.5)	76.3 ± 2.3
0.5321	-2.181 (77.6)	-2.113 (75.3)	-2.009 (77.0)	-1.880 (77.1)	-1.760 (76.1)	76.6 ± 0.9
0.6304	-2.001 (76.9)	-1.942 (73.9)	-1.842 (74.2)	-1.723 (73.7)	-1.612 (71.6)	74.1 ± 1.9
0.7263	-1.826 (72.0)	-1.775 (68.7)	-1.679 (68.4)	-1.570 (67.7)	-1.468 (64.2)	68.2 ± 2.8
0.8198	-1.655 (63.6)	-1.612 (60.3)	-1.520 (58.7)	-1.420 (56.3)	-1.327 (52.9)	58.4 ± 4.1
0.9110	-1.488 (46.0)	-1.454 (43.0)	-1.366 (40.4)	-1.274 (38.8)	-1.190 (36.2)	40.9 ± 3.8
						62 ± 15

<sup>(a)</sup> M%D is mean percentage deviation at each mixture composition calculated according to equation 7. <sup>(b)</sup> These M%D values are overall mean percentage deviations including all compositions.

**Table 4.** Solubility of IMC and EHT calculated by means of Jouyban-Acree model (equations 4 and 5) expressed as decimal logarithm as a function of mixtures composition and temperature. Values in parentheses are percentage deviations calculated according to equation 6.

$f_{AcOEt}$	293.15 K	298.15 K	303.15 K	308.15 K	313.15 K	M%D <sup>(a)</sup>
IMC						
0.1122	-2.282 (6.2)	-2.190 (1.8)	-2.123 (3.7)	-2.029 (3.1)	-1.956 (1.8)	3.3 ± 1.8
0.2214	-2.145 (18.9)	-2.059 (13.1)	-1.994 (14.4)	-1.907 (13.4)	-1.836 (11.1)	14.2 ± 2.9
0.3277	-2.041 (30.4)	-1.960 (27.2)	-1.897 (25.0)	-1.815 (22.8)	-1.747 (19.6)	25.0 ± 4.1
0.4312	-1.955 (39.6)	-1.878 (35.4)	-1.817 (33.7)	-1.740 (30.0)	-1.675 (26.0)	33.0 ± 5.2
0.5321	-1.881 (44.9)	-1.809 (40.8)	-1.749 (37.5)	-1.677 (34.0)	-1.614 (29.4)	37.3 ± 6.0
0.6304	-1.823 (47.6)	-1.755 (44.0)	-1.696 (40.8)	-1.628 (36.3)	-1.567 (30.8)	39.9 ± 6.6
0.7263	-1.789 (47.4)	-1.725 (43.9)	-1.667 (40.5)	-1.603 (36.1)	-1.544 (30.6)	39.7 ± 6.6
0.8198	-1.792 (45.2)	-1.731 (41.1)	-1.674 (38.6)	-1.613 (34.8)	-1.555 (30.1)	38.0 ± 5.8
0.9110	-1.850 (37.5)	-1.791 (34.8)	-1.733 (32.1)	-1.674 (28.8)	-1.616 (25.5)	31.7 ± 4.7
						29 ± 13 <sup>(b)</sup>
EHT						
0.1122	-2.807 (3.6)	-2.705 (3.0)	-2.586 (5.3)	-2.418 (9.7)	-2.260 (23.8)	9.1 ± 8.6
0.2214	-2.525 (13.4)	-2.434 (18.0)	-2.321 (26.6)	-2.165 (38.6)	-2.019 (50.2)	29.4 ± 5.1
0.3277	-2.280 (30.5)	-2.199 (35.2)	-2.091 (44.7)	-1.946 (53.7)	-1.811 (59.8)	44.8 ± 2.2
0.4312	-2.056 (48.6)	-1.984 (46.1)	-1.881 (53.0)	-1.747 (57.4)	-1.622 (58.2)	52.7 ± 5.3
0.5321	-1.848 (51.8)	-1.785 (47.4)	-1.687 (51.7)	-1.564 (52.5)	-1.449 (51.1)	50.9 ± 2.0
0.6304	-1.659 (49.3)	-1.605 (43.3)	-1.511 (44.8)	-1.398 (44.4)	-1.292 (40.7)	44.5 ± 3.1
0.7263	-1.498 (40.4)	-1.452 (34.3)	-1.362 (34.4)	-1.258 (33.7)	-1.161 (27.3)	34.0 ± 4.6
0.8198	-1.377 (31.0)	-1.339 (25.6)	-1.252 (23.3)	-1.156 (19.6)	-1.067 (14.2)	22.8 ± 6.3
0.9110	-1.314 (19.3)	-1.282 (15.3)	-1.197 (12.1)	-1.108 (10.3)	-1.027 (7.0)	12.8 ± 4.7
						33 ± 17 <sup>(b)</sup>

<sup>(a)</sup> M%D is mean percentage deviation at each mixture composition calculated according to equation 7. <sup>(b)</sup> These M%D values are overall mean percentage deviations including all compositions.



**Figure 4.** Logarithmic differences of drugs solubilities [experimental value minus calculated value according to equation 1] for IMC (o) and EHT ( $\Delta$ ) and logarithmic difference of calculated solubilities [value according to J – A model (equation 1) minus value according to equation 1] ( $\square$ ), as a function of the AcOEt proportion in AcOEt + EtOH mixtures at 298.15 K.

Figure 4 shows that differences obtained are positive in all cases and dependent on solvent composition. Thus, experimental solubilities for both compounds are greater than those predicted by equations 1 and 4 (and 5). It is interesting to note that the greatest experimental IMC solubility is found in the same mixture that J – A model predicts the maximum solubility, that is, near to 0.60 in volume fraction of AcOEt. Otherwise, the maximum solubility of EHT is found in the mixture with composition near to 0.50 in volume fraction of AcOEt.

Because the equation 4 (J – A model) is an extension of equation 1, figure 4 shows the excess factor of Jouyban-Acree (J – A Factor), which is equivalent to the logarithmic difference between calculated solubilities by means of both equations, and it is a global excess solubility function.

## CONCLUSIONS

The generated solubility data of two drugs in ethyl acetate + ethanol mixtures at various temperatures extend the available database of solubility data of pharmaceuticals (31) which is in high demand in the industry. From all topics discussed previously it follows that IMC and EHT experimental solubilities present positive deviations in front to those predicted by the Jouyban-Acree model in the AcOEt + EtOH binary solvent system at all compositions studied. These estimation

differences are within 30% as mean for both drugs which makes possible the use of the J – A model if these differences are allowed along the different stages of design and development of new products in the pharmaceutical and cosmetic industries.

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Carrera 75 No. 65-87 Bloque 44 aula 209 Teléfono: 219 92 33 Fax: 230 50 07  
Medellín - Colombia  
labsensorial@pijaos.udea.edu.co - extfacqf@farmacia.udea.edu.co

